

GT Power Simulation of the Influence of Exhaust Manifold Design on Sound Quality

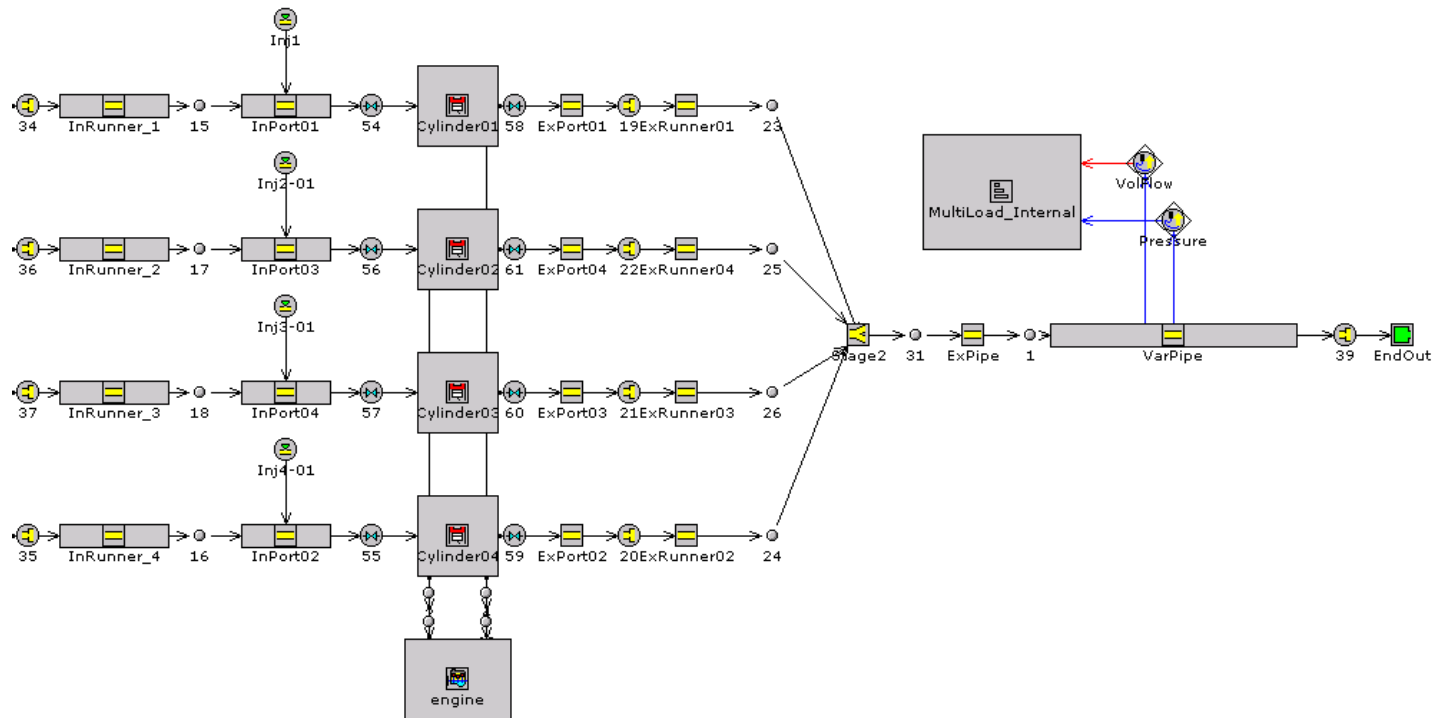
Ivan Arbuckle

Emcon Technologies

GT Power User Conference – Detroit 2009

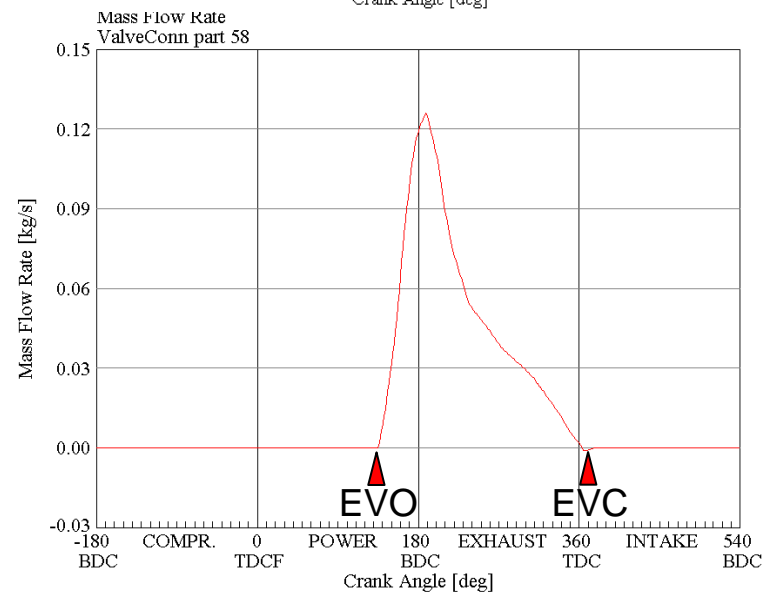
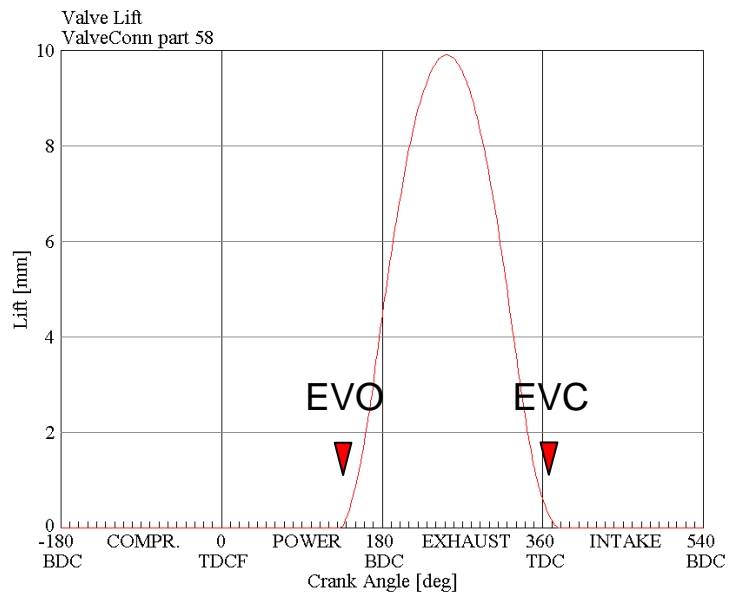
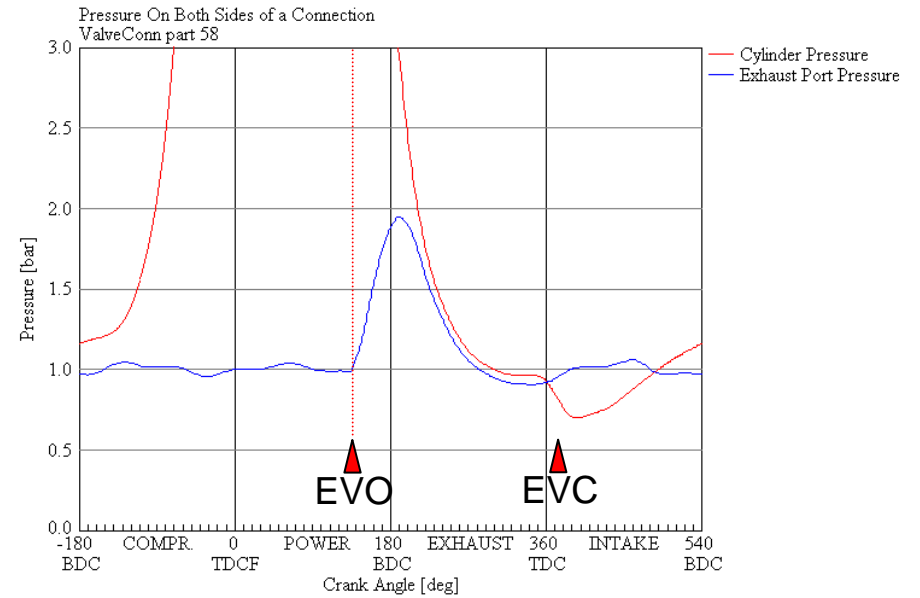
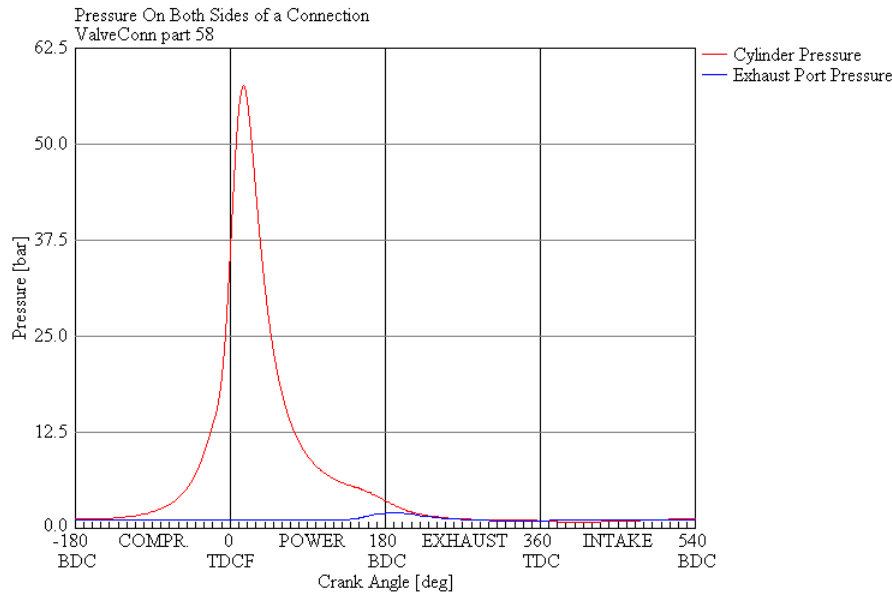
■ Objective

- Study the exhaust manifold design factors that influence noise
 - Asymmetry
 - Restriction
 - Cylinder-Cylinder Interference
- Characterize the Engine Noise Source Characteristics
 - Ps and Zs from the MultiLoad Template

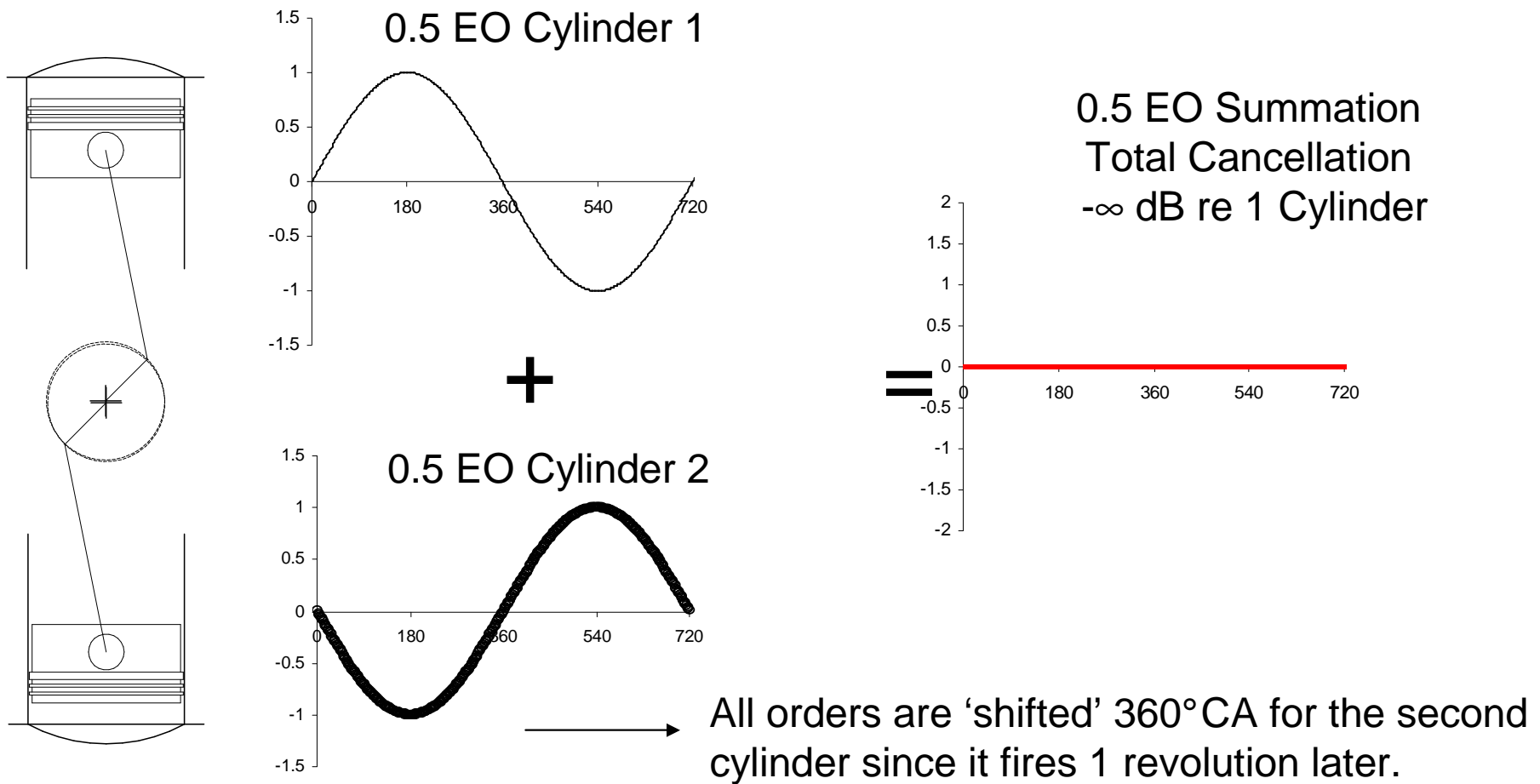


Why is there noise in the Exhaust?

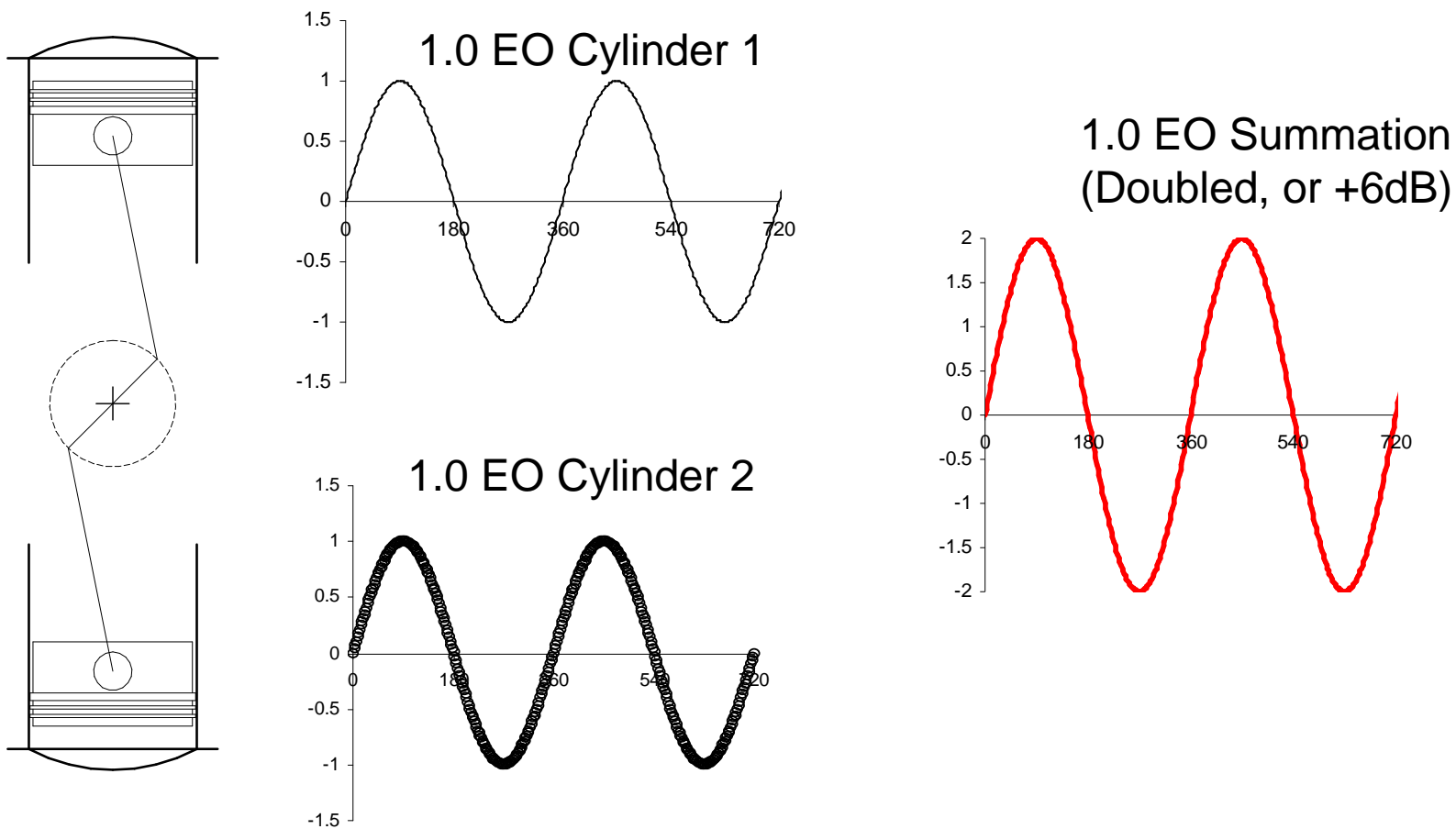
- The noise is caused by the unsteady mass flow rate from the engine. This leads to oscillations in the exhaust pipe which are emitted at the outlet as tail pipe noise.
- If the flow from the engine was a steady (non oscillating) flow there would be no order noise.



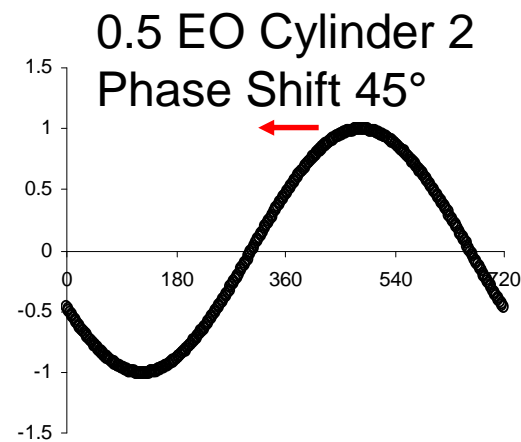
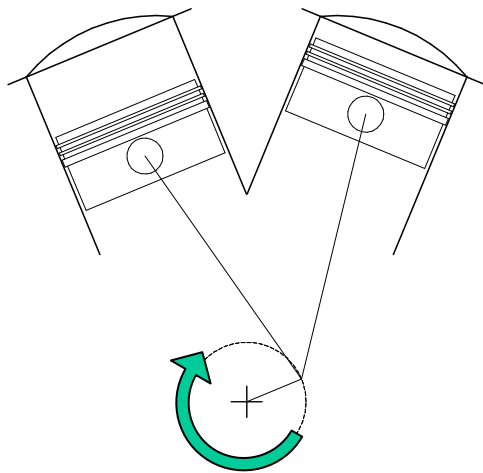
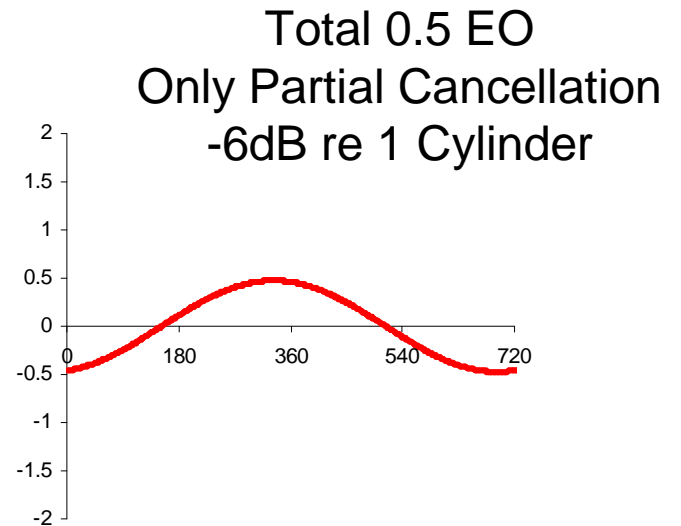
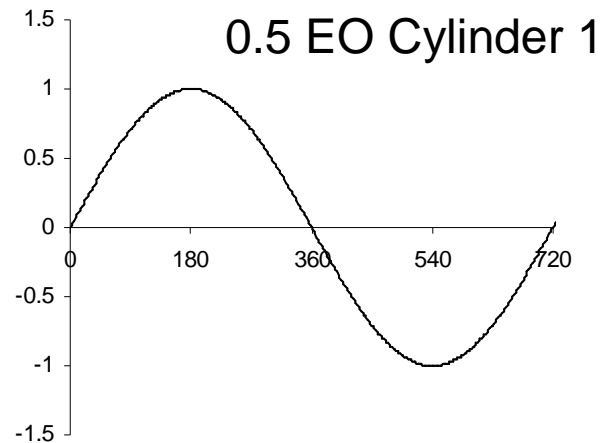
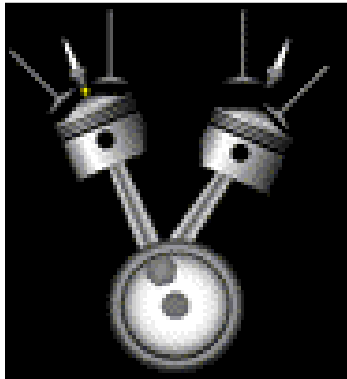
Why is 0.5 OE suppressed in a 2 cylinder engine ?



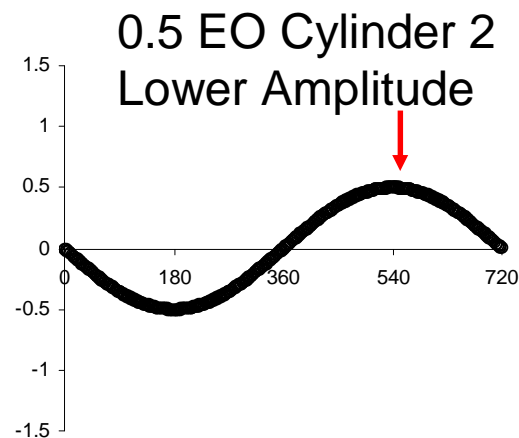
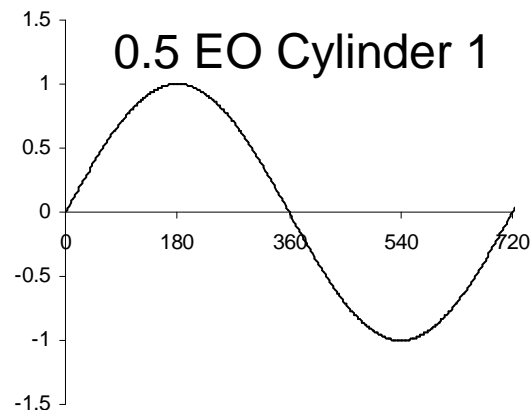
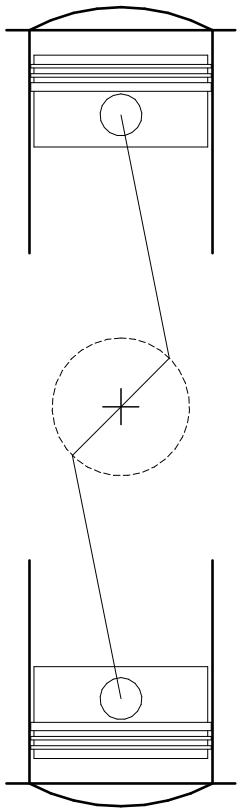
Why is 1 EO not suppressed in a 2 cylinder engine ?



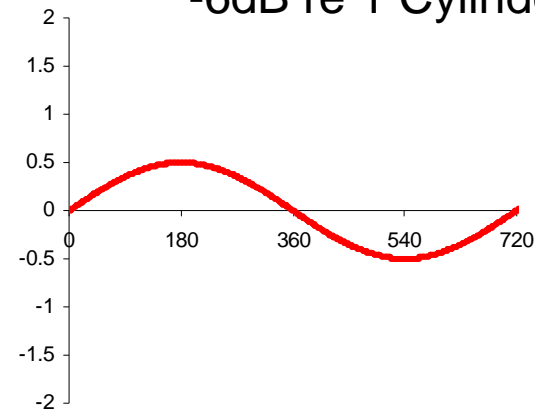
What if firing is not 360° separated for a twin cylinder ?



What else can cause incomplete 0.5 EO Cancellation ?



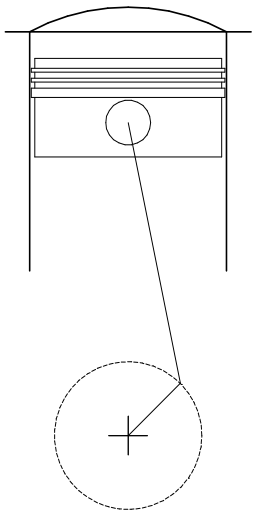
Total 0.5 EO
Only Partial Cancellation
-6dB re 1 Cylinder



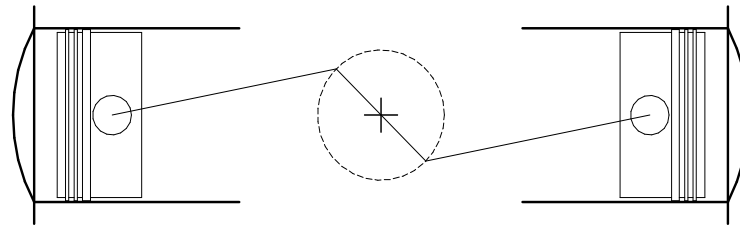
An amplitude shift can be caused by;

- incomplete combustion in 1 cylinder
- inconsistent cylinder-to-cylinder V_{eff}
- or imbalanced restriction in exhaust manifolds.

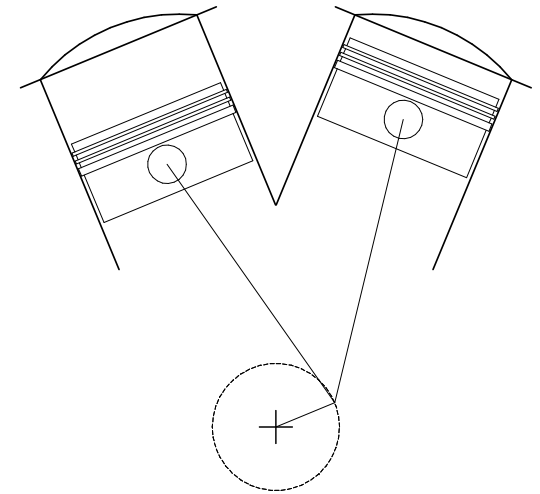
Singles & Twins



Single Cylinder
(4 Stroke)

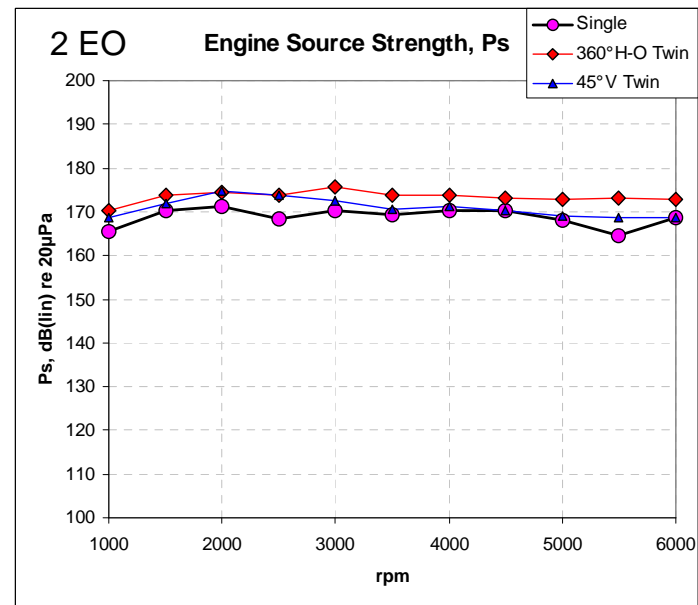
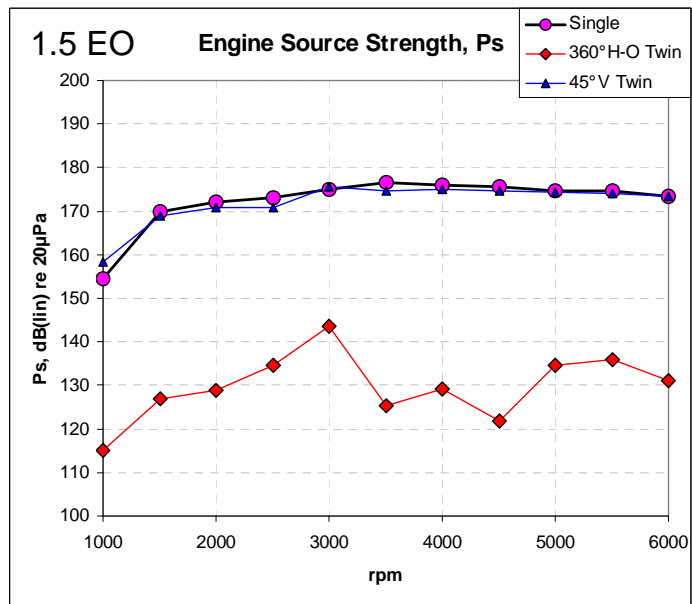
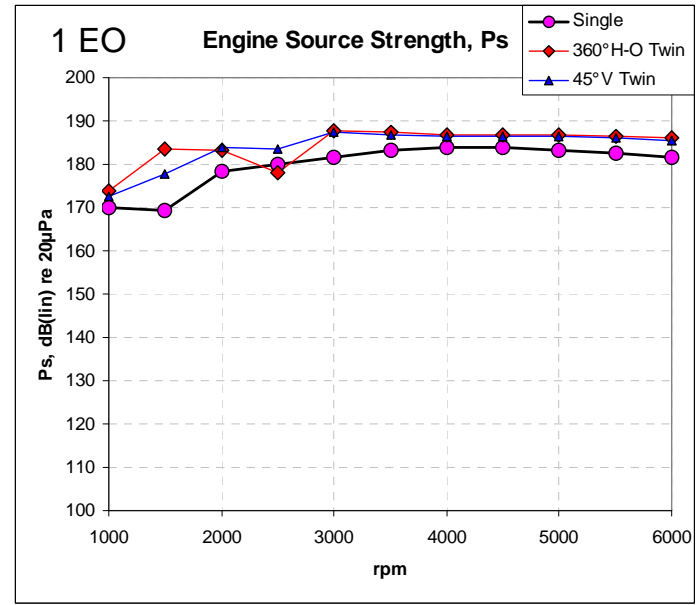
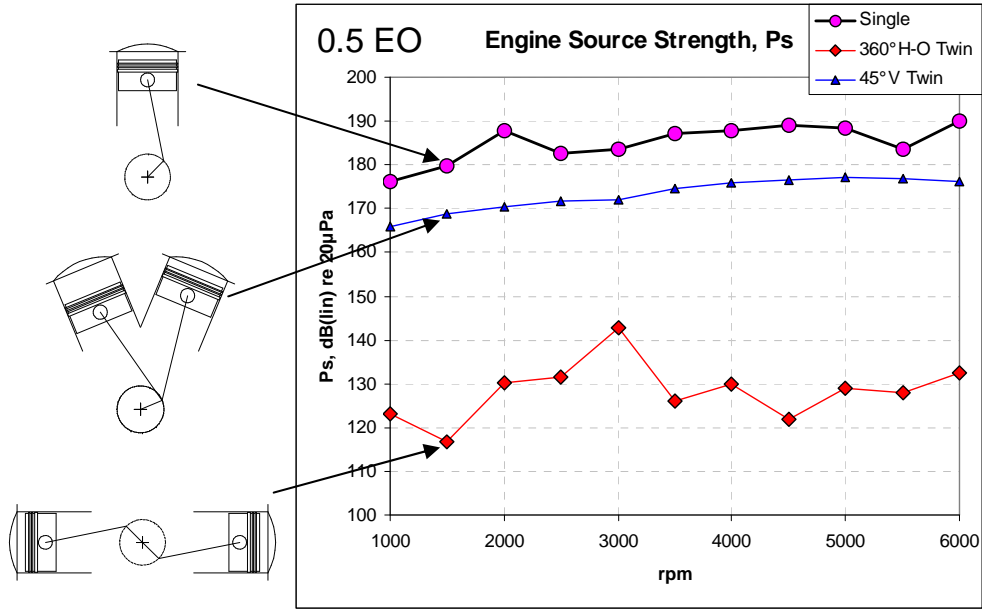


Horizontally
Opposed Twin
(360° Firing)

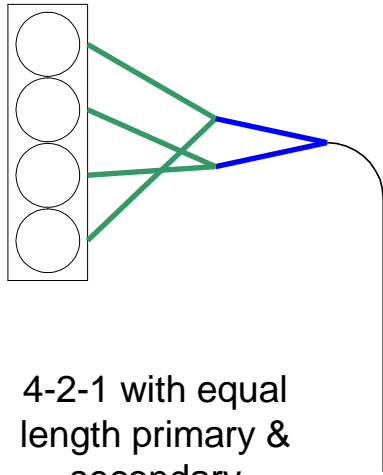


45° V Twin
Common
Crank Throw
(405°-315°)

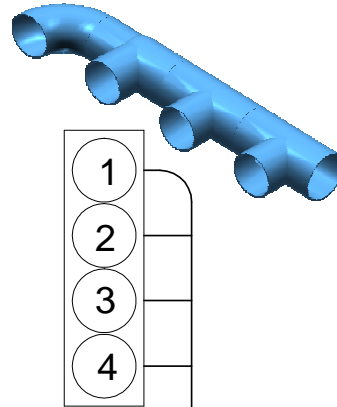
Singles & Twins: Source Level (Ps)



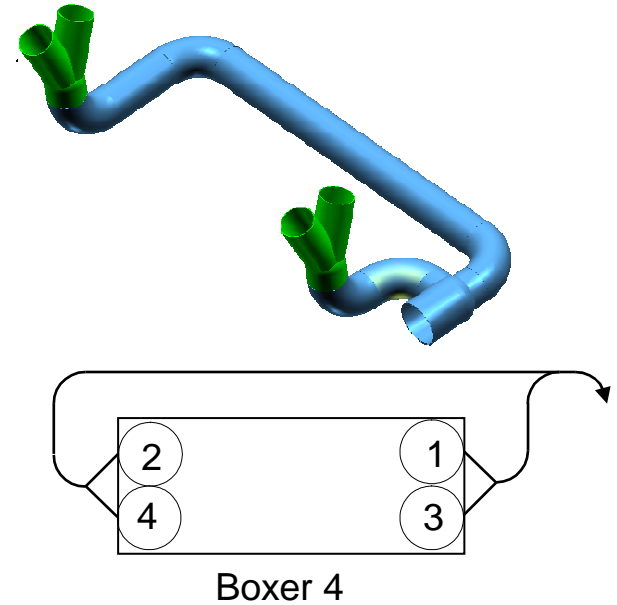
4 Cylinder (Firing 1-2-4-3)



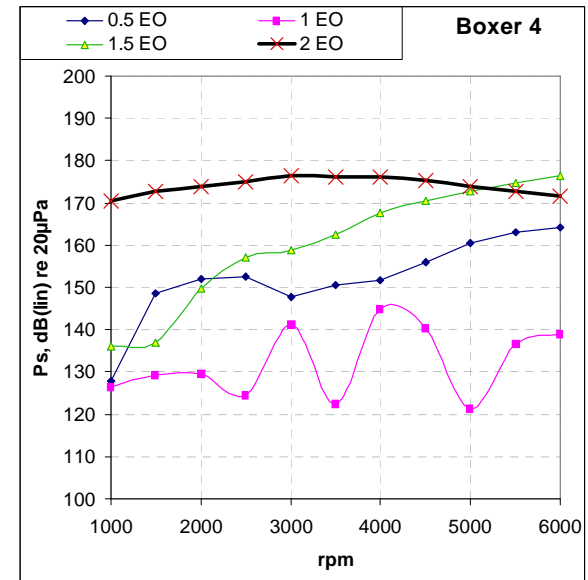
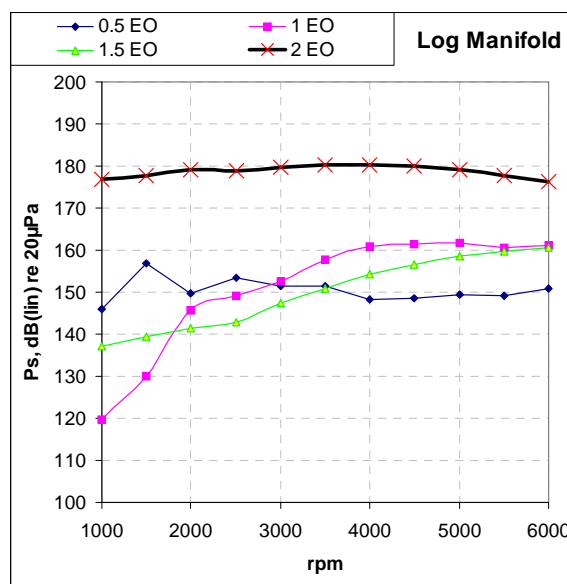
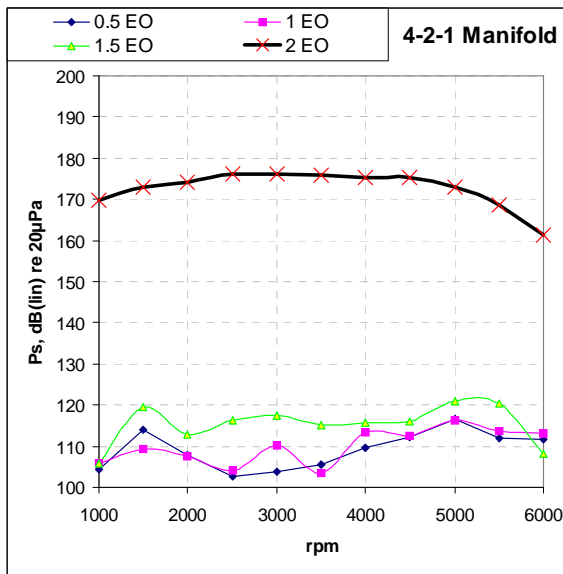
4-2-1 with equal length primary & secondary



14 with Log Manifold



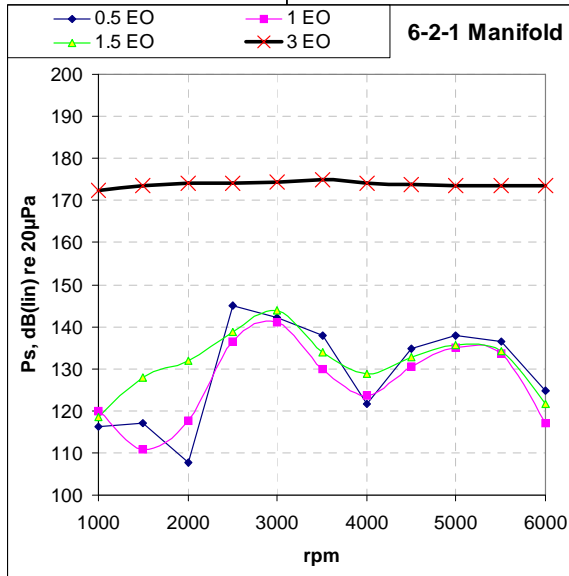
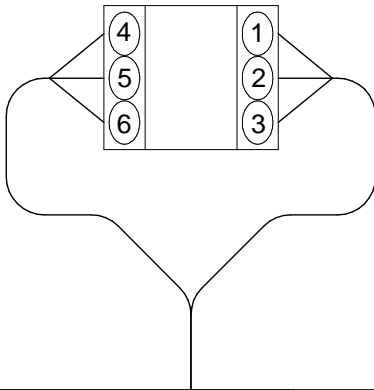
Boxer 4



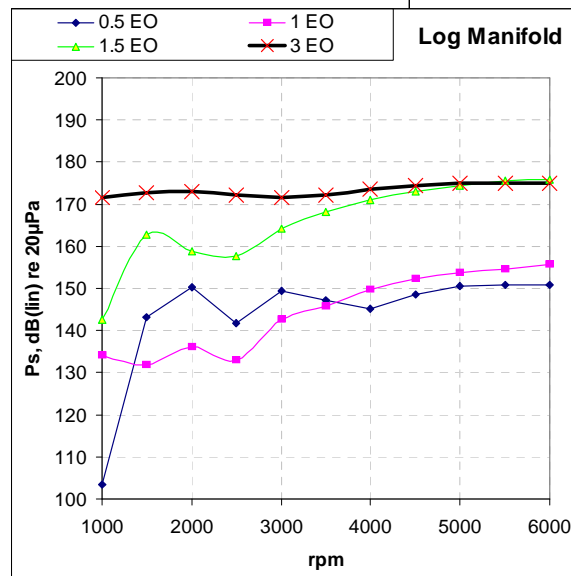
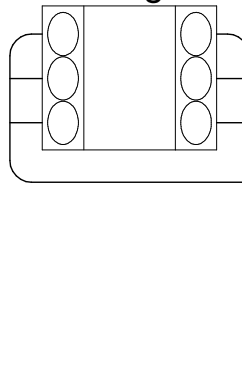
V6

(Firing 1-4-2-5-3-6 = R-L-R-L-R-L)

6-2-1 Symmetrical

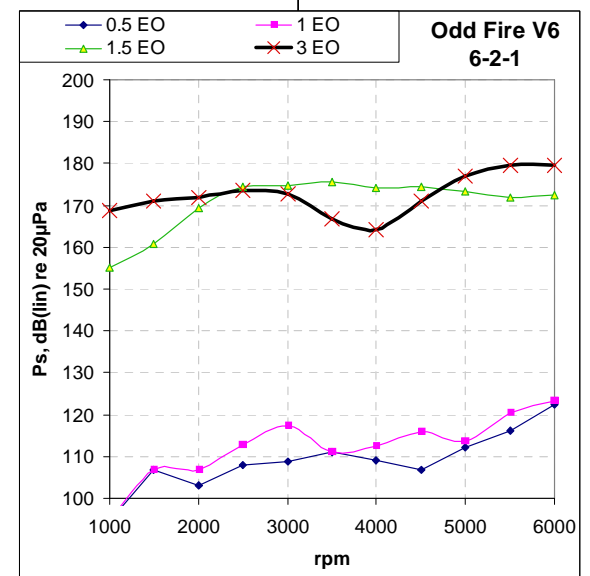
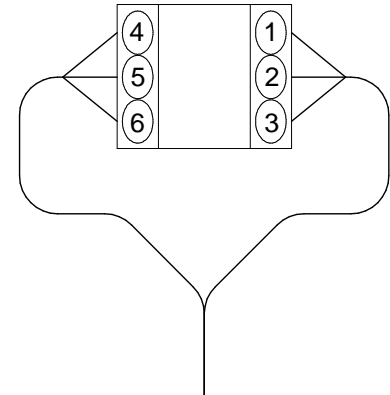


Asymmetric Log



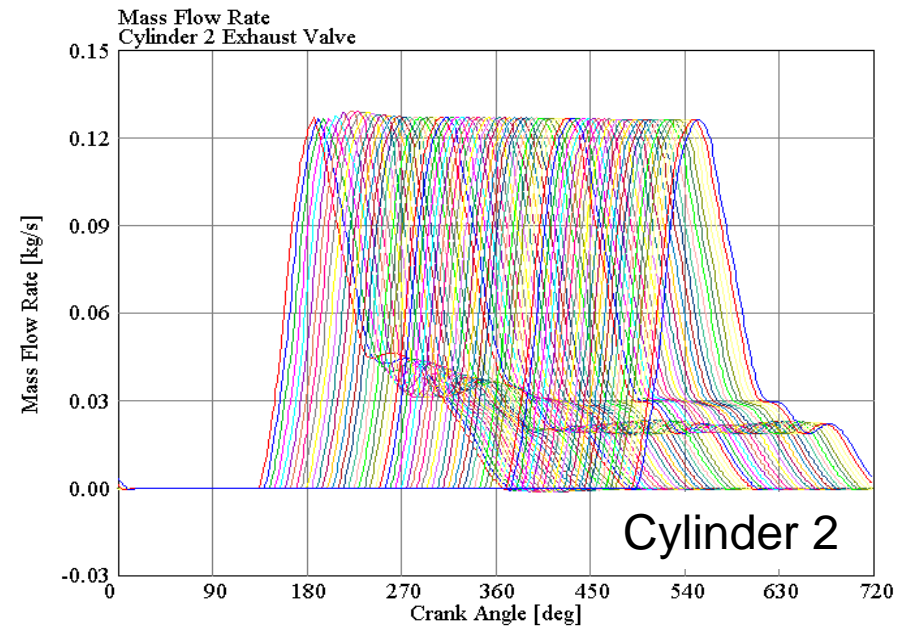
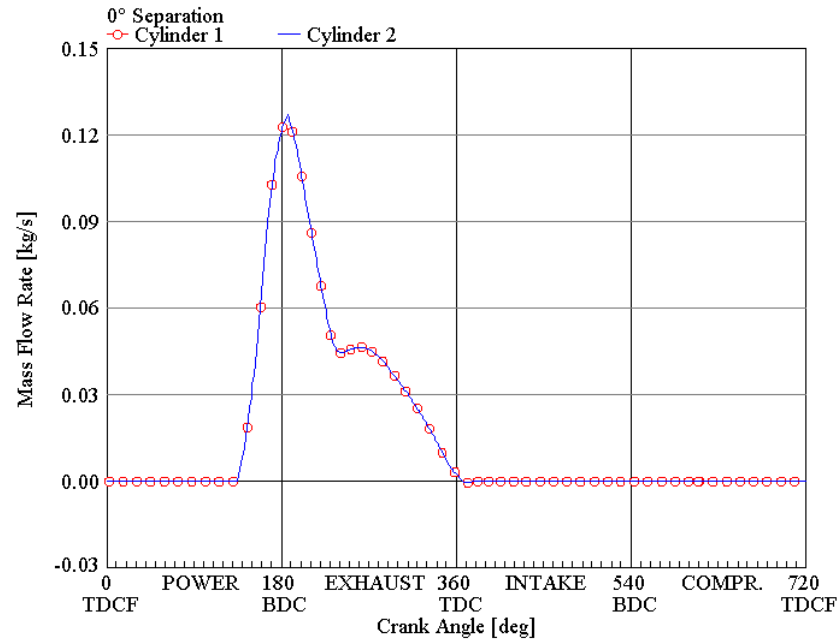
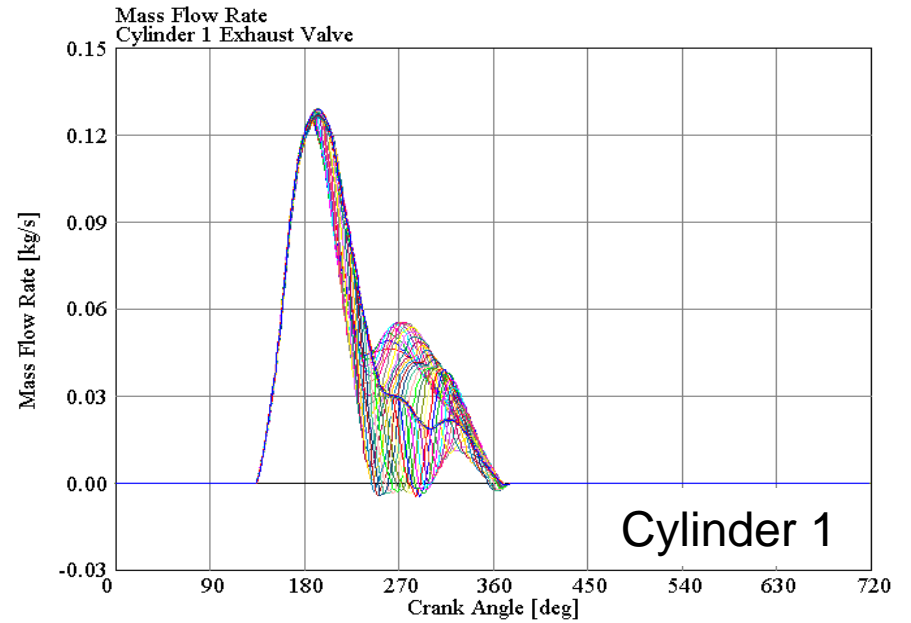
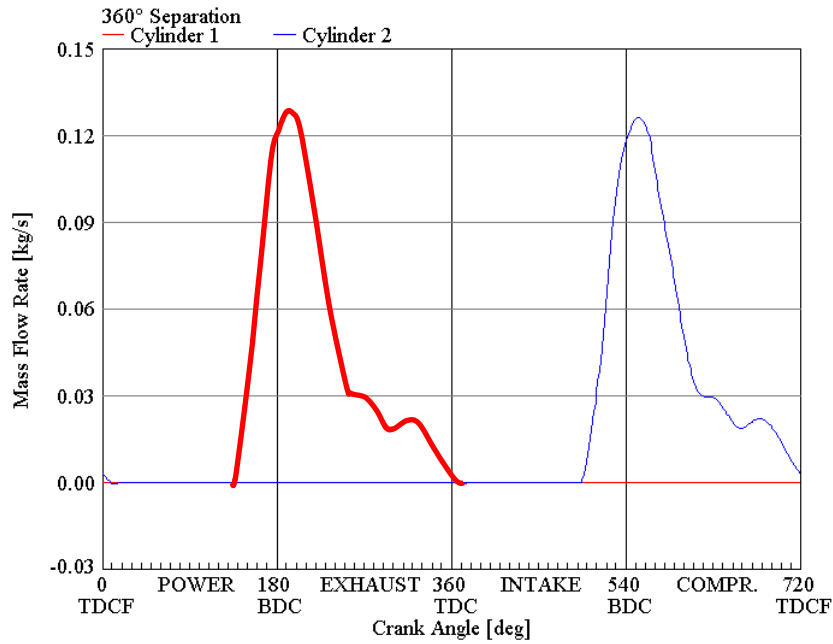
90° V6

Firing 90°-150°-90°-150°-90°-150°





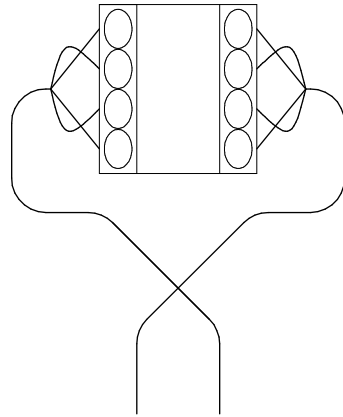
EMCON Technologies Cylinder Interference in Twin Cylinder Engines



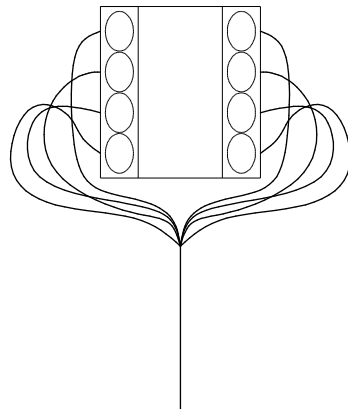
Cross Plane V8

(Firing 1-3-7-2-6-5-4-8 = R-R-L-R-L-L-R-L)

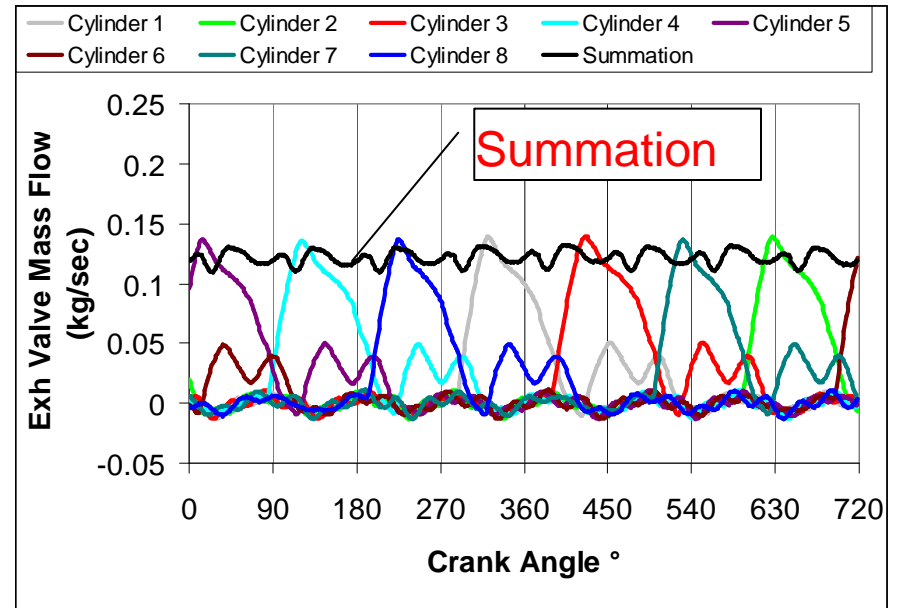
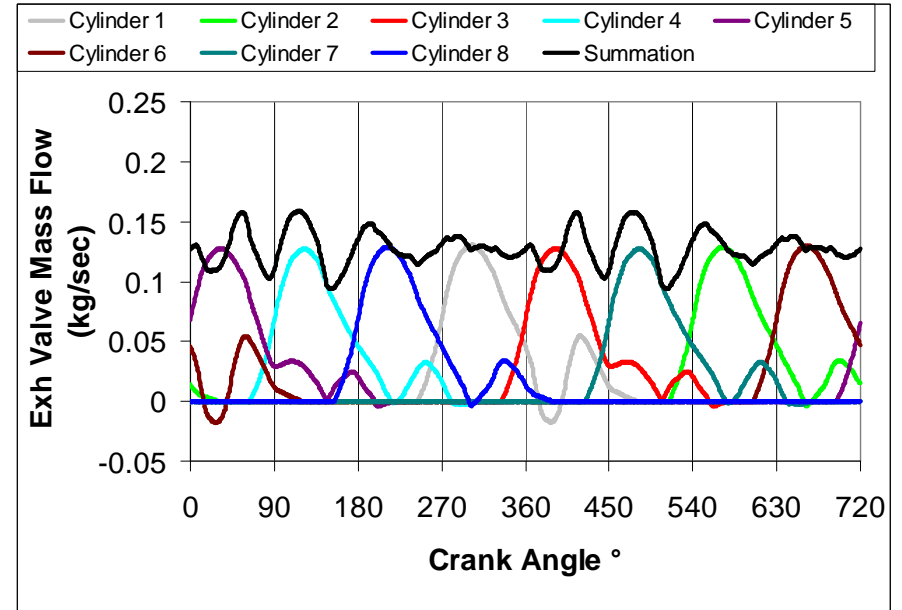
8-2-X-2



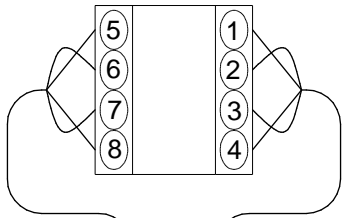
Symmetrical
8-1 Manifold



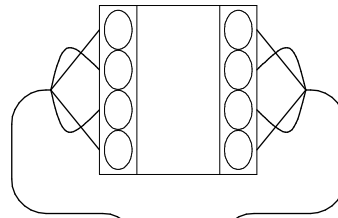
Uneven bank-to-bank firing on a cross-plane crank V8 causes variation from cylinder to cylinder. A 8-1 manifold can overcome this (as can a flat plane crank).



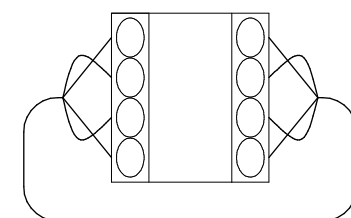
V8 (Firing 1-3-7-2-6-5-4-8)



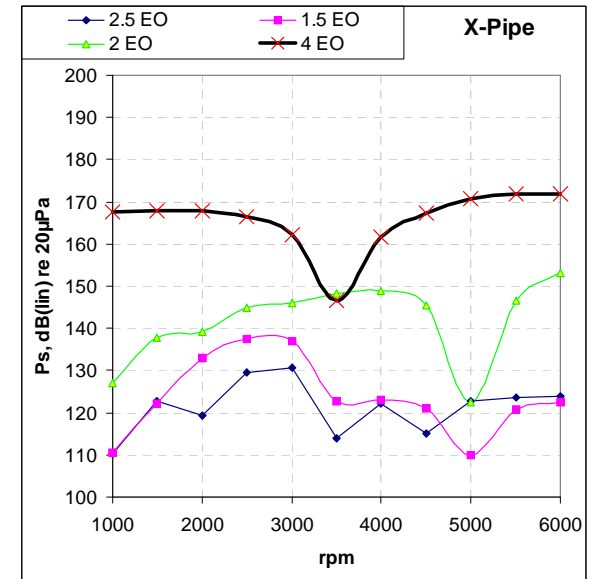
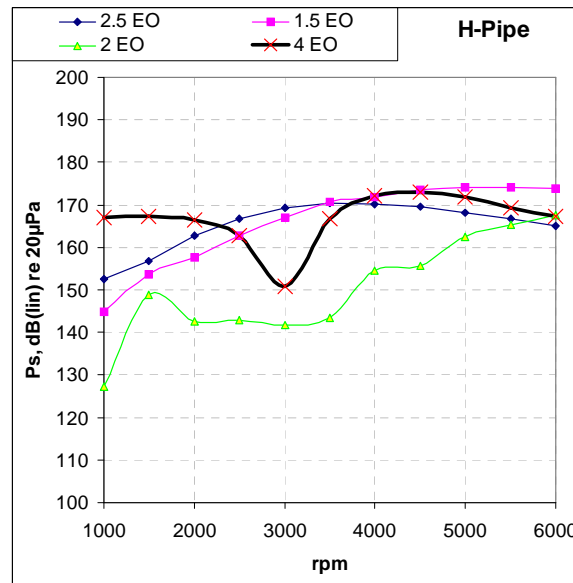
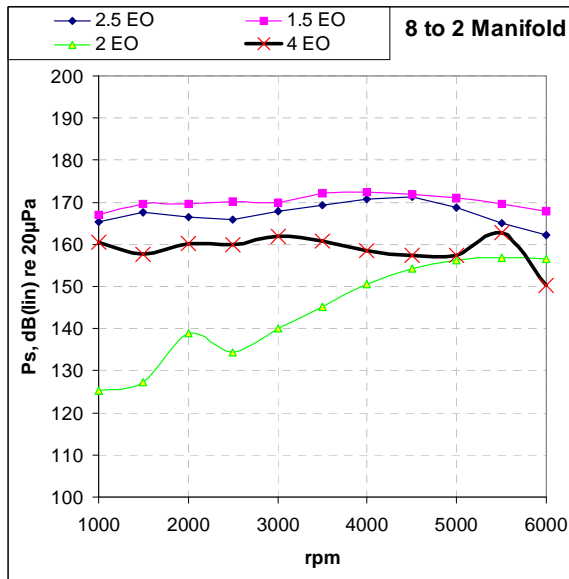
Dual V8 – No Bank-to-Bank mixing.



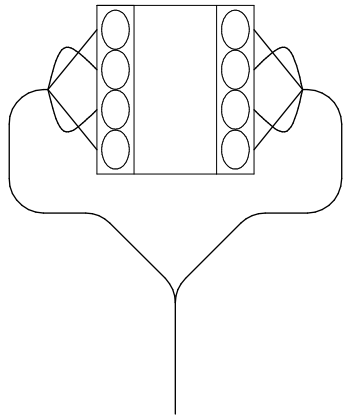
H-Pipe V8 with equal length primary



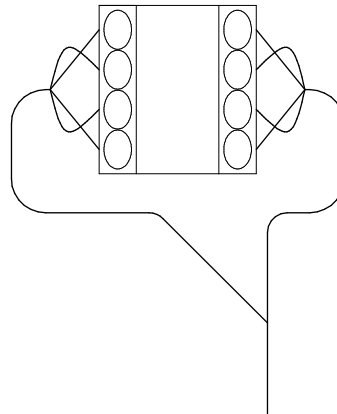
X-Pipe V8 with equal length primary



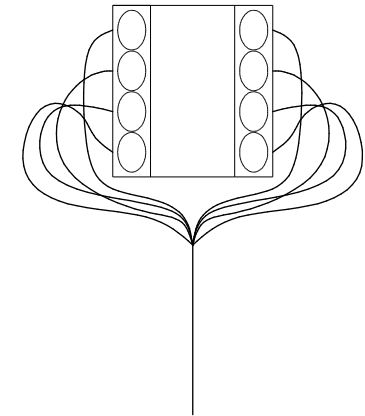
V8 (Firing 1-3-7-2-6-5-4-8)



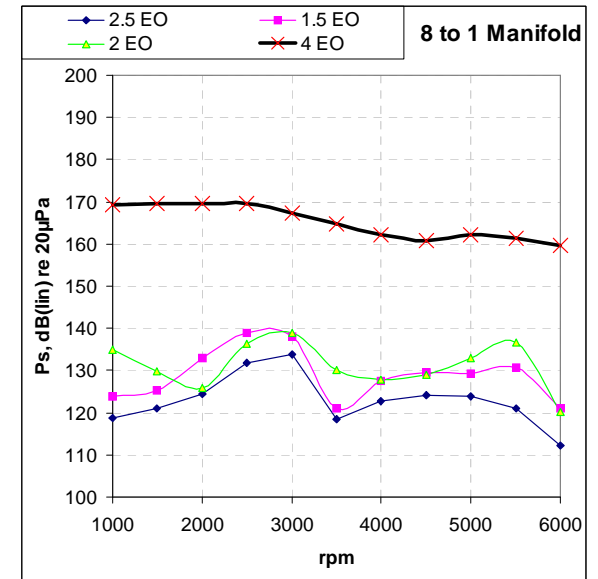
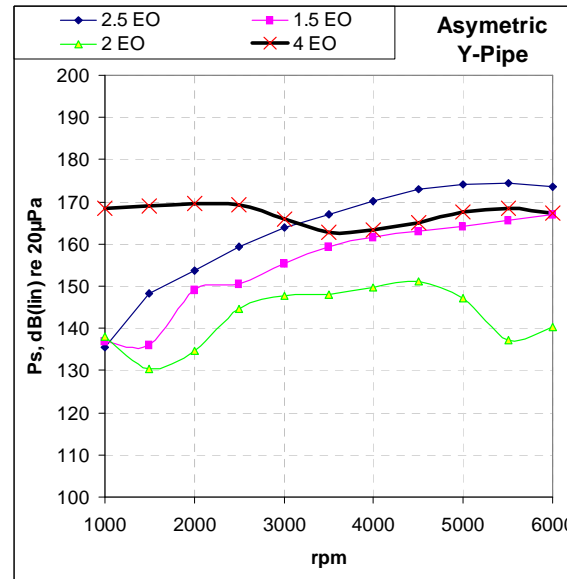
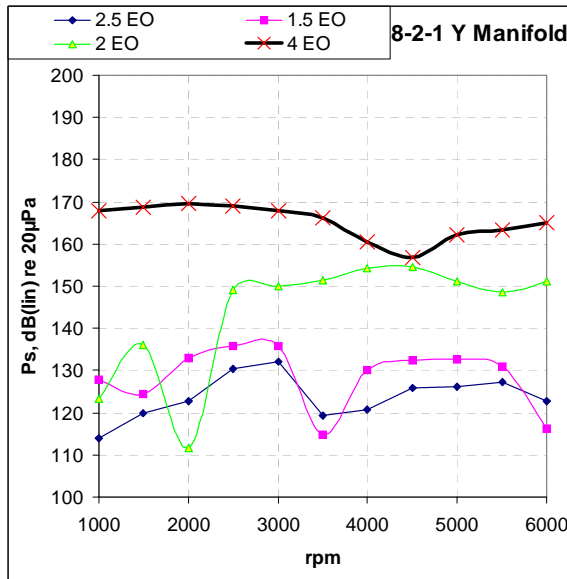
Y-Pipe V8 with equal length primary



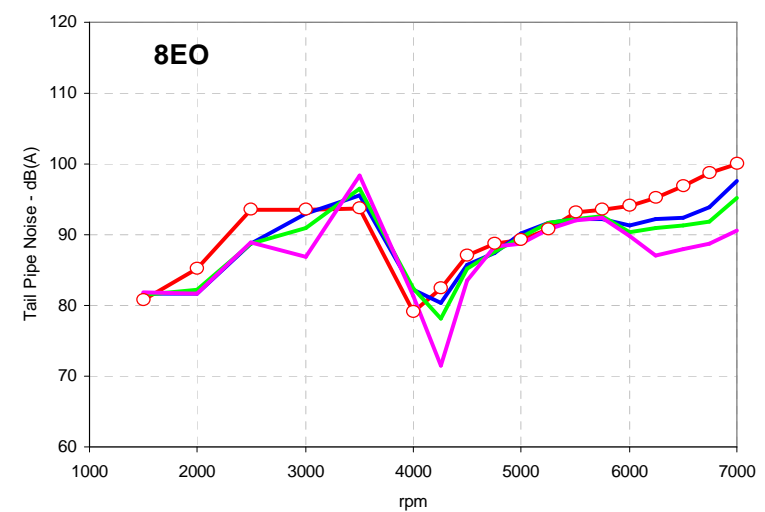
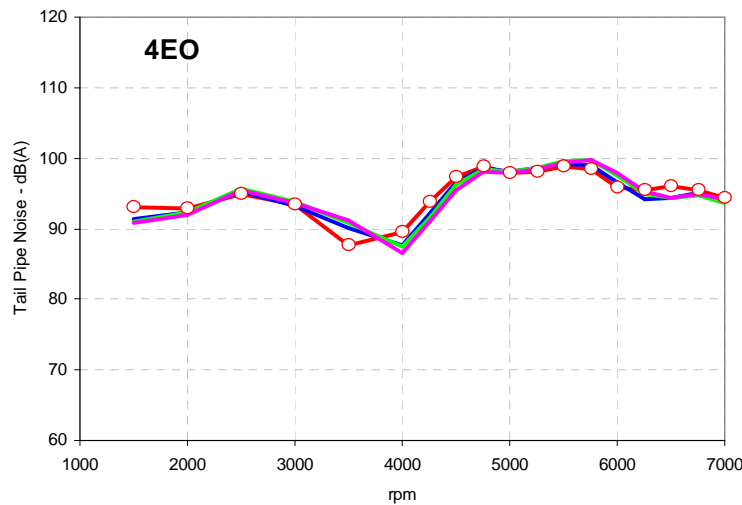
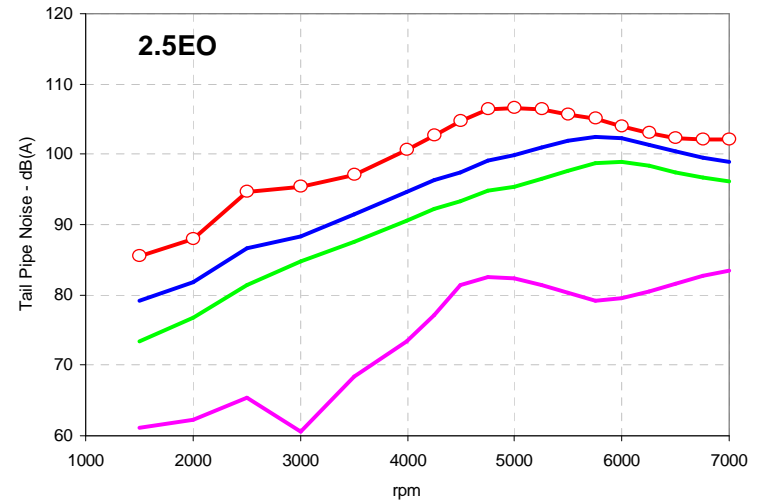
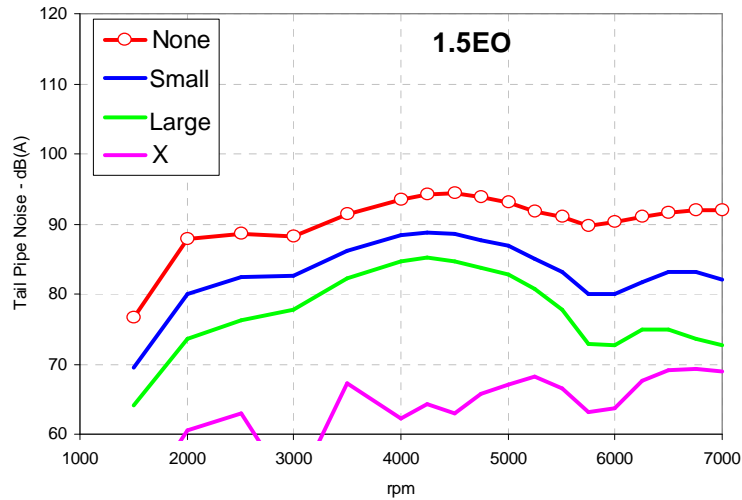
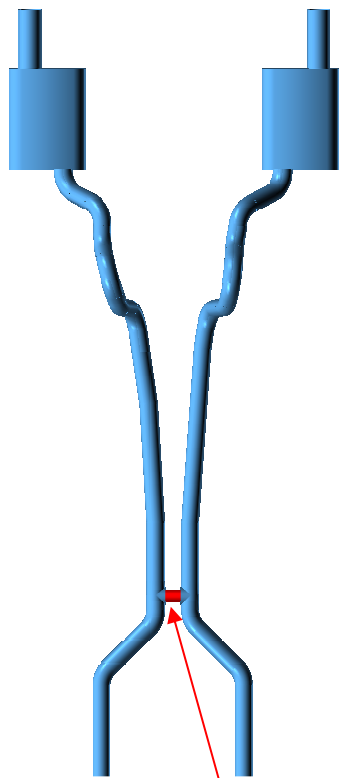
Y-Pipe V8 with equal primary, Unequal Secondary



8-into-1 V8 with equal length primary



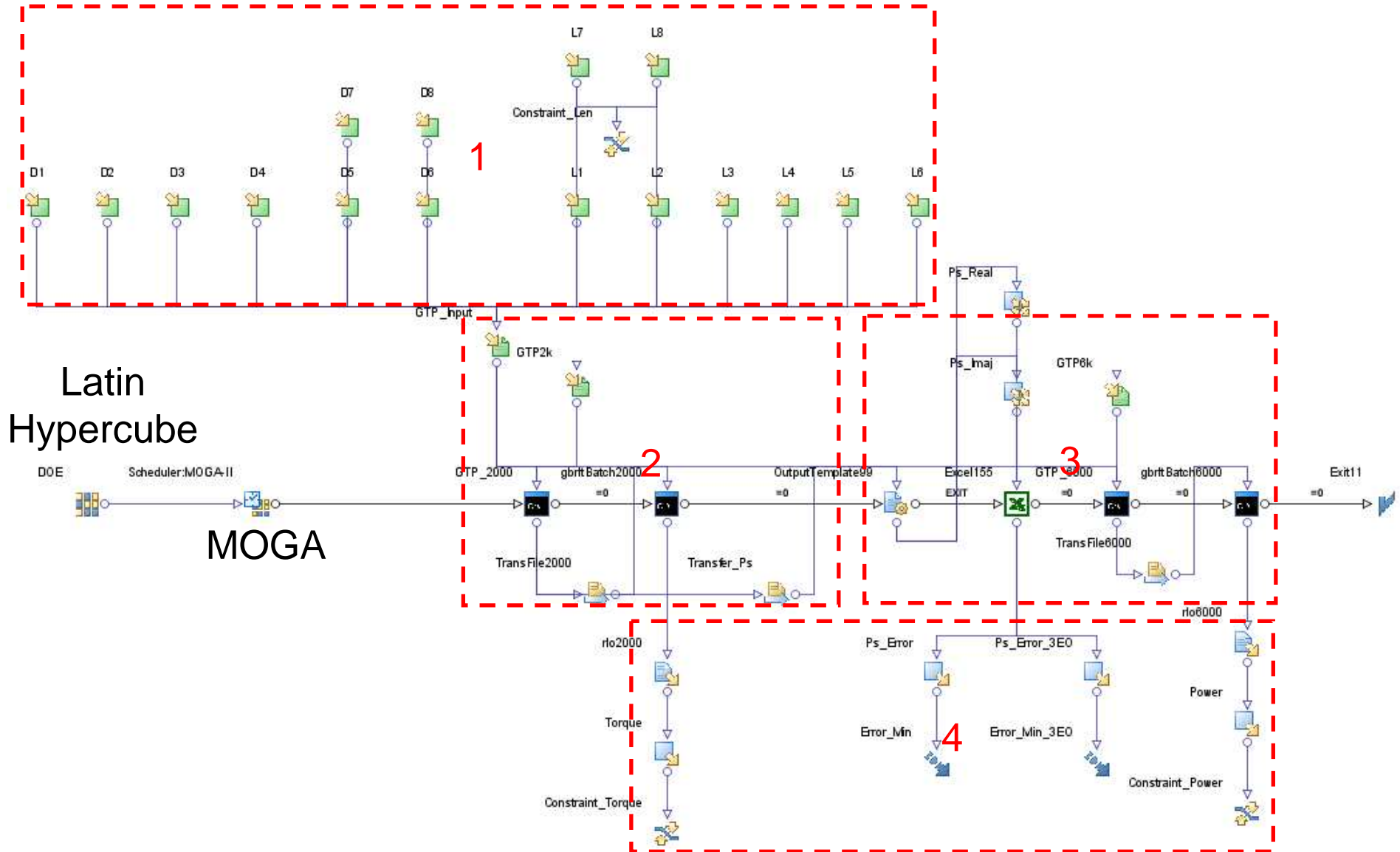
H-Pipe 'Tuning' on a V8 Application



Varying the H-pipe diameter can have a large affect on half order levels.

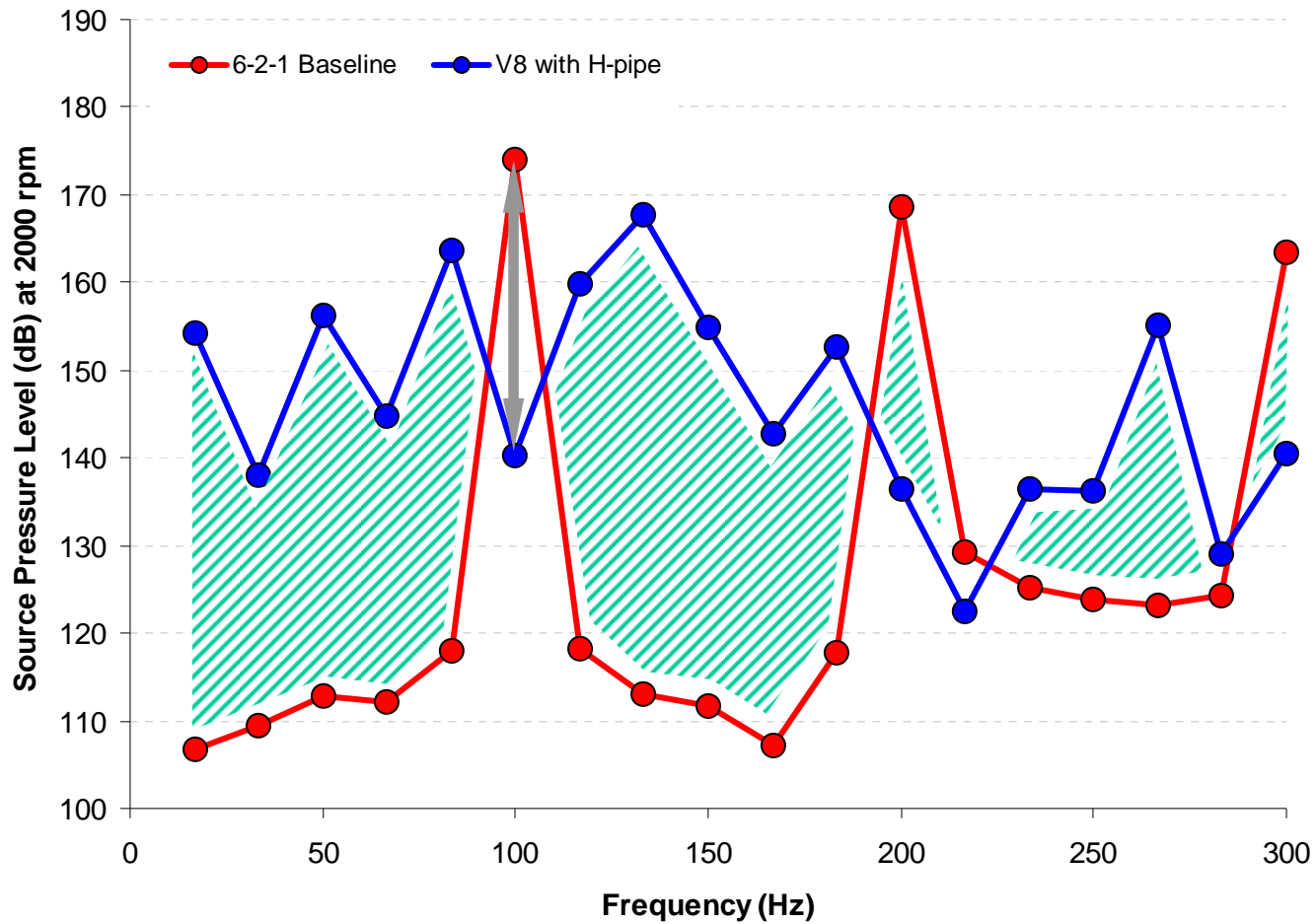
This is used as another tuning parameter to achieve the best sound quality.

modeFrontier Optimization V6→V8 : Work Flow



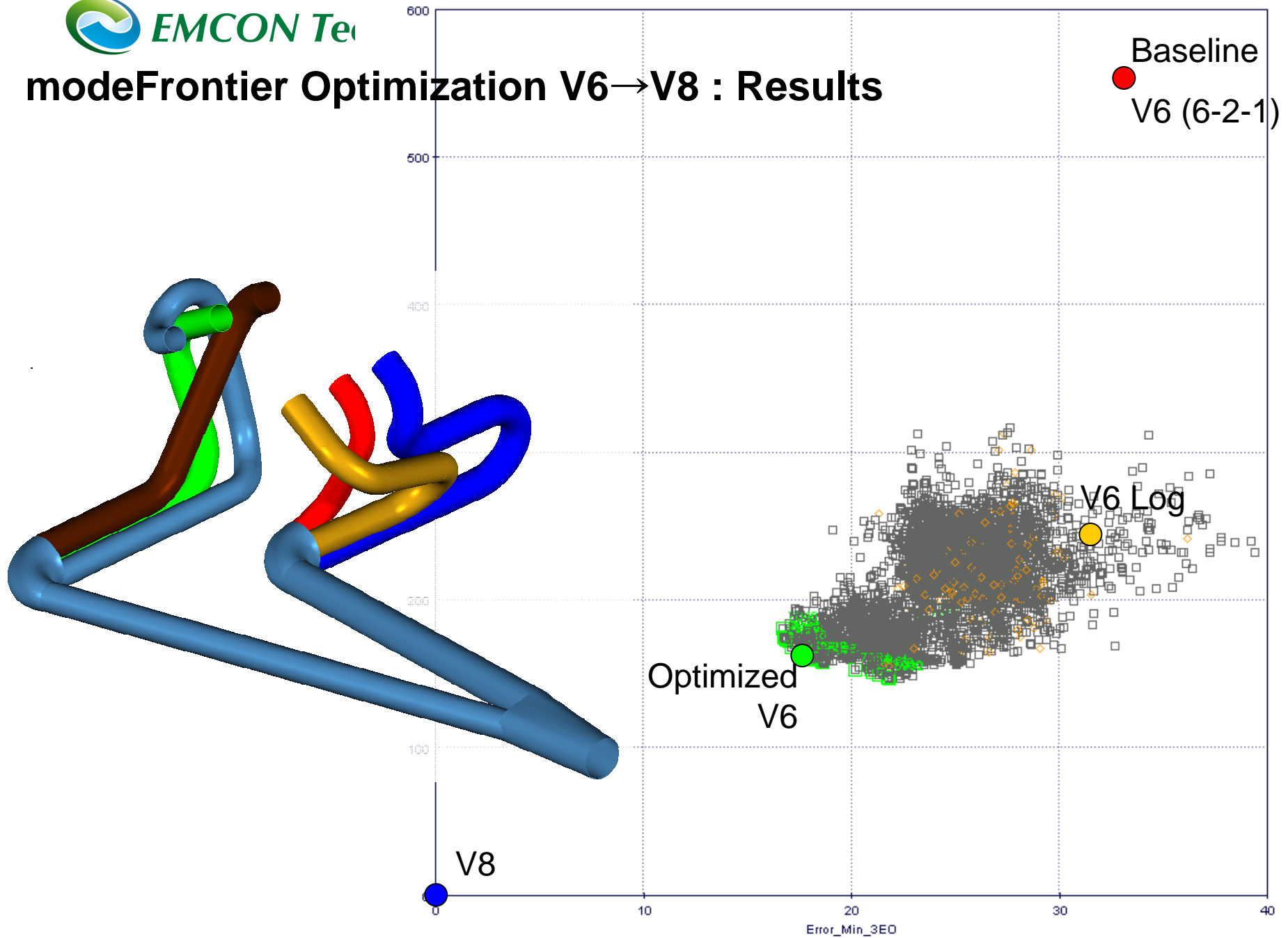
modeFrontier Optimization V6→V8 : Targets

Ps at 2000 rpm





modeFrontier Optimization V6→V8 : Results



Conclusions

Multi-Cylinder Engines have the potential to significantly suppress half orders

But there are many design features which can re-introduce half order content;

Engine Factors

- Odd-Fire Engine
- Even Fire engine with Odd-Fire on each bank

Manifold Factors

- Length Differences - introduces phase errors
- Restriction Differences - introduces amplitude errors
- Inadequate Bank-to-Bank Mixing